

I. Introduction to Numerical Methods

A. Conventions

1. In optics and photonics, both physicists and engineers work. The conventions are a mix of both.
2. Additionally, computer algorithms are usually based on standard computer science/mathematics conventions in packages such as Matlab, NAG, IMSL, Linpack, Eispack, etc.

! } Thus, workers who are doing computing
 . } must be aware of all three conventions
 and know how to translate among them

3. This difference is found in my group's work
 - a. Most of our papers are based on the physics convention
 - b. OCS is based on the math/CS convention, which is close to the engineering convention.

4. The basic difference

Let $u(x, t)$ be a waveform that is the sum of a finite number of waves. In that case:

a. Physics convention:

$$u(z, t) = \sum_{n=1}^N A_n \cos(k_n z - \omega_n t + \phi_n)$$

k_n = wavenumber, ω_n = frequency, z = distance,
 t = time, A_n = amplitude, ϕ_n = phase
 N = positive integer.

b. Mathematics convention:

$$u(z, t) = \sum_{n=1}^N A_n \cos(\omega_n t + k_n z + \phi_n)$$

Note that this is equivalent
 to backward propagation

c. Engineering convention

$$u(z, t) = \sum_{n=1}^{\infty} A_n \cos\left(2\pi\nu_n t - \frac{2\pi}{\lambda_n} z + \phi_n\right)$$

[But also $\omega_n = 2\pi\nu_n$
 $\beta_n = 2\pi/\lambda_n$]

The sign change in going from the physics convention to the engineering/mathematics/CS may appear trivial, but it has many important ramifications.

It is usual to express these sums using complex exponentials

a. Physics convention

$$u(z, t) = \sum_{n=1}^N a_n \exp[i(k_n z - \omega_n t)]$$

b. Mathematics convention

$$u(z, t) = \sum_{n=1}^N a_n \exp[i(\omega_n t + k_n z)]$$

c. Engineering convention

$$u(z, t) = \sum_{n=1}^N a_n \exp\left[2\pi j\left(\nu_n t - \frac{z}{\lambda_n}\right)\right]$$

$i = \sqrt{-1}$ (mathematicians and physicists)

$j = \sqrt{-1}$ (engineers)

6. Continuous limit

a. Physics convention

$$u(z, t) = \int_{-\infty}^{\infty} \frac{d\omega}{2\pi} A(\omega) \exp[i(kz - \omega t)]$$

Sometimes this factor is left out

(Why the factor of 2π ? You will see)

b. Mathematics convention

$$u(z, t) = \int_{-\infty}^{\infty} \frac{d\omega}{2\pi} A(\omega) \exp[i(\omega t + kz)]$$

c. Engineering convention

$$u(z, t) = \int_{-\infty}^{\infty} d\nu A(\nu) \exp\left[2\pi j\left(\nu t - \frac{1}{\lambda} z\right)\right]$$

Factor of 2π allows us to directly connect $A(\omega)$ and $A(\nu)$: $A_\omega(\omega) = A_\nu(2\pi\nu)$

The functions are not the same!

7. Dispersion relations

a. The relationship between k and ω is fixed by the dispersion relationship: $k = k(\omega)$, which is a property of the medium

In vacuum: $k(\omega) = \omega/c$

More generally: $k(\omega) = \omega n(\omega)/c$

In glass fibers, $n(\omega)$ is a slowly varying function in the neighborhood of $\lambda_0 = 1.5 \mu$ and $n(\omega = 2\pi c/\lambda_0) \approx 1.5$. Note: λ_0 is the wavelength outside the glass and equals $\omega/2\pi c$!

b. In communications signals, the signal bandwidth is always small compared to the carrier frequency



However, we normally cut off this part and consider only positive frequencies. If $k(\omega)$ varies slowly, then we can Taylor expand $k(\omega)$ we must put it back when considering nonlinearity

Note: Negative frequencies must be present if $u(z,t)$ is real.

$$k(\omega) - k(\omega_0) = \left. \frac{dk}{d\omega} \right|_{\omega_0} (\omega - \omega_0) + \frac{1}{2} \left. \frac{d^2k}{d\omega^2} \right|_{\omega_0} (\omega - \omega_0)^2 + \frac{1}{6} \left. \frac{d^3k}{d\omega^3} \right|_{\omega_0} (\omega - \omega_0)^3 + \dots$$

We can remove the carrier frequency by writing

(1) Physics convention:

$$u(z, t) = \bar{u}(z, t) \exp[ik_0 z - i\omega_0 t]$$

(2) Mathematics convention

$$u(z, t) = \bar{u}(z, t) \exp(i\omega_0 t + ik_0 z)$$

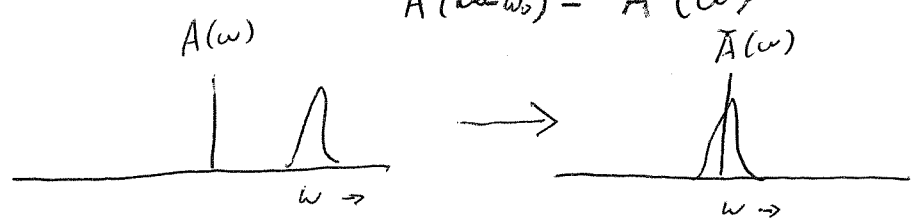
(3) Engineering convention

$$u(z, t) = \bar{u}(z, t) \exp(j\omega_0 t - j\beta_0 z)$$

[Replace ν, λ with ω, β]

We now translate $A(\omega) : \bar{A}(\omega)$

$$\bar{A}(\omega - \omega_0) = A(\omega)$$



C. We now find: physics convention

$$\bar{u}(z, t) = \int_{-\infty}^{\infty} \frac{d\omega}{2\pi} \bar{A}(\omega - \omega_0) \exp\{i[k(\omega) - k_0]z - i(\omega - \omega_0)t\}$$

(1.6)

Letting $\Omega = \omega - \omega_0$, $K(\Omega) = k(\omega_0 + \Omega) - k_0$,
 we find $\approx K_0' \Omega + \frac{1}{2} K_0'' \Omega^2 + \frac{1}{6} K_0''' \Omega^3 + \dots$

$$\bar{u}(z, t) = \int_{-\infty}^{\infty} \frac{d\Omega}{2\pi} \bar{A}(\Omega) \exp\{i[K(\Omega)z - \Omega t]\}$$

d. We can now derive a propagation equation:

$$\frac{\partial \bar{u}(z, t)}{\partial z} = \int_{-\infty}^{\infty} \frac{d\Omega}{2\pi} [iK(\Omega)] \bar{A}(\Omega) \exp\{i[K(\Omega)z - \Omega t]\}$$

$$= \int_{-\infty}^{\infty} \frac{d\Omega}{2\pi} \left[iK_0' \Omega + \frac{i}{2} K_0'' \Omega^2 + \frac{i}{6} K_0''' \Omega^3 \right]$$

$$\cdot \exp\{i[K(\Omega)z - \Omega t]\}$$

$$= -K_0' \frac{\partial \bar{u}(z, t)}{\partial t} - \frac{i}{2} K_0'' \frac{\partial^2 \bar{u}(z, t)}{\partial t^2}$$

$$+ \frac{i}{6} K_0''' \frac{\partial^3 \bar{u}(z, t)}{\partial t^3} + \dots$$

or:

$$i \frac{\partial \bar{u}(z, t)}{\partial z} + iK_0' \frac{\partial \bar{u}(z, t)}{\partial t} - \frac{i}{2} K_0'' \frac{\partial^2 \bar{u}(z, t)}{\partial t^2} - \frac{i}{6} K_0''' \frac{\partial^3 \bar{u}(z, t)}{\partial t^3} + \dots = 0$$

Dropping the bars and returning to k

$$i \frac{\partial u(z, t)}{\partial z} + i k_0' \frac{\partial u(z, t)}{\partial t} - \frac{i}{2} k_0'' \frac{\partial^2 u(z, t)}{\partial t^2}$$

$$- \frac{i}{6} k_0''' \frac{\partial^3 u(z, t)}{\partial t^3} + \dots = 0$$

e. We now subtract the group velocity motion

$$t' = t - k_0' z; \quad z' = z$$

$$i \frac{\partial u(z, t)}{\partial z} - \frac{1}{2} k_0'' \frac{\partial^2 u(z, t)}{\partial t^2} - \frac{i k_0'''}{6} \frac{\partial^3 u(z, t)}{\partial t^3} + \dots = 0$$

where we have dropped the primes.

f. Other conventions:

(1) Mathematics convention

$$i \frac{\partial u(z, t)}{\partial z} - \frac{1}{2} k_0'' \frac{\partial^2 u(z, t)}{\partial t^2} + \frac{i k_0'''}{6} \frac{\partial^3 u(z, t)}{\partial t^3}$$

$$+ \dots = 0$$

(2) Engineering convention β_0''

$$j \frac{\partial u(z, t)}{\partial z} + \frac{1}{2} \beta_0'' \frac{\partial^2 u(z, t)}{\partial t^2} - \frac{j \beta_0'''}{6} \frac{\partial^3 u(z, t)}{\partial t^3}$$

$$+ \dots = 0$$

→ Insert on transformation refs.

8. Polarization conventions

a. In a birefringent medium — and all fibers have some birefringence — there are two dispersion relations $k_+(w)$ and $k_-(w)$, (which differ by about 1 part in 10^6 in fibers)

7A. Transforming between conventions

$$a. \quad u_{\text{physics}}(z, t) = u_{\text{math}}(z, -t)$$

It is just a sign reversal of time

In OCS, you would make this change at the input and output

$$\text{Note: } a_{\text{physics}}(z, \omega) = \int_{-\infty}^{\infty} dt \, u_{\text{physics}}(z, t) \exp(i\omega t)$$

$$= \int_{-\infty}^{\infty} dt \, u_{\text{math}}(z, -t) \exp(i\omega t) \quad t \rightarrow -t'$$

$$= \int_{-\infty}^{\infty} dt \, u_{\text{math}}(z, t') \exp(-i\omega t')$$

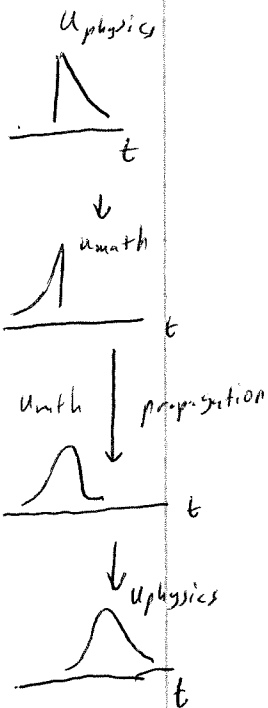
$$= a_{\text{math}}(z, \omega)$$

There is no change in the spectrum because in the physics convention one defines the Fourier transform with the opposite sign from the math and physics conventions

$$b. \quad u_{\text{eng}}(z, t) = u_{\text{physics}}^*(z, t) = u_{\text{math}}^*(z, -t)$$

$$a_{\text{eng}}(z, \omega) = a_{\text{physics}}^*(z, \omega) = a_{\text{math}}^*(z, \omega)$$

because of sign change in the definition of the Fourier transform



1.7B

7B. Who uses what convention?

Math convention: OCS at present
This convention is consistent with
standard math packages like Matlab

Physics convention: Agrawal, Born and Wolf,
Our research group

Engineering convention: Haus (always),
Kazavsky, Benedetto, and Wilner
(except chap. 7 - watch out -
compare chaps. 6 and 7)
Most of the engineering literature.

1.8

In the x and y direction with the physics convention

$$u_x = A_+ \cos \theta \exp [i(k_+ z - \omega t) + i\phi_1] + A_- \sin \theta \exp [i(k_- z - \omega t) + i\phi_2]$$

$$u_y = -A_+ \sin \theta \exp [i(k_+ z - \omega t) - i\phi_2] + A_- \cos \theta \exp [i(k_- z - \omega t) - i\phi_1]$$

$$\begin{pmatrix} u_x \\ u_y \end{pmatrix} = \begin{pmatrix} \cos \theta e^{i\phi_1} & \sin \theta e^{i\phi_2} \\ -\sin \theta e^{-i\phi_2} & \cos \theta e^{-i\phi_1} \end{pmatrix} \begin{pmatrix} A_+ e^{ik_+ z} \\ A_- e^{ik_- z} \end{pmatrix}$$

$$\text{Let } \beta = (\phi_1 + \phi_2)/2, \quad \gamma = (\phi_1 - \phi_2)/2 \quad \left\{ \begin{array}{l} \text{we let} \\ \delta = 0 \\ \rightarrow \text{constant offset} \end{array} \right.$$

$$S_0 = |u_x|^2 + |u_y|^2 = A_+^2 + A_-^2$$

$$S_1 = |u_x|^2 - |u_y|^2 = (A_+^2 - A_-^2) \cos 2\theta + 2A_+ A_- \sin 2\theta \cos [(\Delta k)z + 2\gamma]$$

$$S_2 = 2 \operatorname{Re}(u_x u_y^*) = -(A_+^2 - A_-^2) \sin 2\theta \cos(2\beta) - 2A_+ A_- \sin(2\beta) \sin(\Delta k z + 2\gamma) + 2A_+ A_- \cos(2\beta) \cos 2\theta \cos(\Delta k z + 2\gamma)$$

$$S_3 = 2 \operatorname{Im}(u_x u_y^*) = -(A_+^2 - A_-^2) \sin 2\theta \sin(2\beta) + 2A_+ A_- \cos(2\beta) \sin(\Delta k z + 2\gamma) + 2A_+ A_- \sin(2\beta) \cos 2\theta \cos(\Delta k z + 2\gamma)$$

which is a circle on a sphere of radius $A_1^2 + A_2$

- b. It is normal to refer to a polarization state as right-handed when it advances clockwise when approaching the observer

That occurs when $S_3 > 0$

Conversely, light is referred to as left-handed when it advances counter-clockwise when approaching the observer, which occurs when $S_3 < 0$.

- c. In the engineering convention, just the opposite is true. However, in a recent article by Gordon and Kogelnik, just the opposite is true, they change the convention, so that the sign of S_3 is changed.

- d. The mathematics convention is more subtle. Perhaps the best way to think of it is as equivalent to the physics convention once we set $t \rightarrow -t$.