

Modeling phase noise in high-power photodetectors

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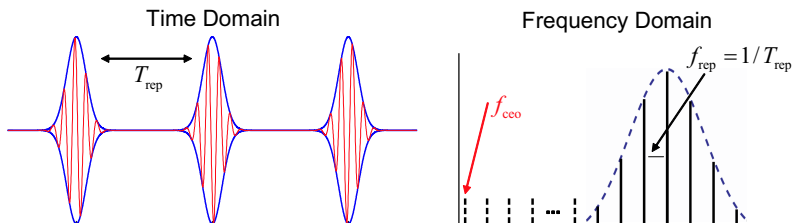


Background

In 1999–2000: Frequency combs were invented

“The excitement surrounding the rapid evolution in these fields since 1999 gives us a hint of what it must have been like after 1927 when the first ideas of quantum mechanics were introduced. . .”

— J. L. Hall and T. W. Hänsch, 2005 Nobel prize winners in Physics



The key advance was electronically locking f_{ceo} and f_{rep} !



Prior work

- Phase noise in photodetectors limits applications in
 - RF-photonics
 - time and frequency metrology
- ★ Quinlan et al.¹ theoretically predicted:
 - phase noise from a train of ultrashort optical pulses tends to zero as the optical pulse width tends to zero
- ★ Quinlan et al.² experimentally observed:
 - this decrease ceases once the optical pulse width becomes small compared to the electrical pulse width
- ★ Sun et al.³ reproduced the experimental results using Monte Carlo simulations
- Monte Carlo simulations are too computationally slow to be used for performance optimization and physical insight is lost

¹F. Quinlan et al., J. Opt. Soc. Am. B **30**, 1775–1785 (2013).

²F. Quinlan et al., Nat. Photonics **7**, 290–293 (2013).

³W. Sun et al., Phys. Rev. Lett. **113**, 203901 (2014).



This Work

- We use the drift-diffusion equations instead of Monte Carlo simulations
 - This approach takes minutes on a desktop computer, as opposed to hours on a computer cluster
- We explain analytically that the mean-square phase noise tends to a constant non-zero value when the optical pulse width tends to zero
- We use our approach to design an optimized device



Structure of the MUTC photodetector we model

<i>p</i> -region	InGaAs, p+, Zn, 2.0×10^{19} , 50 nm	50 nm
	InP, p+, Zn, 1.5×10^{18} , 100 nm	150 nm
	InGaAsP, Q1.1, Zn, 2.0×10^{18} , 15 nm	165 nm
	InGaAsP, Q1.4, Zn, 2.0×10^{18} , 15 nm	180 nm
	InGaAs, p, Zn, 2.0×10^{18} , 100 nm	280 nm
	InGaAs, p, Zn, 1.2×10^{18} , 150 nm	430 nm
	InGaAs, p, Zn, 8.0×10^{17} , 200 nm	630 nm
	InGaAs, p, Zn, 5.0×10^{17} , 250 nm	880 nm
<i>i</i> -region	InGaAs, Si, 1.0×10^{16} , 150 nm	1030 nm
	InGaAsP, Q1.4, Si, 1.0×10^{16} , 15 nm	1045 nm
	InGaAsP, Q1.1, Si, 1.0×10^{16} , 15 nm	1060 nm
	InP, Si, 1.4×10^{17} , 50 nm	1110 nm
	InP, Si, 1.0×10^{16} , 900 nm	2010 nm
<i>n</i> -region	InP, n+, Si, 1.0×10^{18} , 100 nm	2110 nm
	InP, n+, Si, 1.0×10^{19} , 900 nm	3010 nm
	InGaAs, n+, Si, 1.0×10^{19} , 20 nm	3030 nm
	InP, n+, Si, 1.0×10^{19} , 200 nm	3230 nm
	InP, semi-insulating substrate Double side polished	

→ Cliff layer

MUTC structure fabricated by Li et al.¹

¹Z. Li et al., IEEE J. Quantum Electron. **46**, 626–632 (2010).



Drift-Diffusion Model

$$\frac{\partial n}{\partial t} = G_{\text{opt}} + G_{\text{ii}} - R(n, p) + \frac{\nabla \cdot \mathbf{J}_n}{q}$$

$$\frac{\partial p}{\partial t} = G_{\text{opt}} + G_{\text{ii}} - R(n, p) - \frac{\nabla \cdot \mathbf{J}_p}{q}$$

$$0 = \nabla \cdot \nabla \varphi + \frac{q}{\epsilon} (N_D^+ + p - n - N_A^-)$$

n	electron density	p	hole density
G_{opt}	optical generation rate	G_{ii}	impact ionization generation rate
R	recombination rate	φ	electric potential
\mathbf{J}_n	electron current density	\mathbf{J}_p	hole current density
N_D^+	donor density	N_A^-	acceptor density



Drift-Diffusion Model

$$\mathbf{J}_p = qp\mathbf{v}_p(\mathbf{E}) - qD_p(\mathbf{E})\nabla p, \quad \mathbf{J}_n = qn\mathbf{v}_n(\mathbf{E}) + qD_n(\mathbf{E})\nabla n$$

$$G_{ii} = \alpha_n \frac{|\mathbf{J}_n|}{q} + \alpha_p \frac{|\mathbf{J}_p|}{q}, \quad G_{\text{opt}} = G_c \exp[-\alpha(L-x)]$$

$$G_c = Q\alpha, \quad Q = \frac{P}{A}$$

\mathbf{v}_n electron drift velocity

D_n electron diffusion coefficient

G_c generation rate coefficient

L device length

A the area of the light beam

α_n electron impact ionization coefficient

\mathbf{v}_p hole drift velocity

D_p hole diffusion coefficient

α absorption coefficient

x distance across the device

P the power of the light beam

α_p hole impact ionization coefficient



Drift velocity model

Empirical expressions that have been used to fit $\mathbf{v}_n(\mathbf{E})$ for electrons¹ and $\mathbf{v}_p(\mathbf{E})$ for the holes² are given by

$$\mathbf{v}_n(\mathbf{E}) = \frac{\mathbf{E} (\mu_n + v_{n,\text{sat}}\beta|\mathbf{E}|)}{1 + \beta|\mathbf{E}|^2}, \quad \mathbf{v}_p(\mathbf{E}) = \frac{\mu_p v_{p,\text{sat}} \mathbf{E}}{(v_{p,\text{sat}}^\gamma + \mu_p^\gamma |\mathbf{E}|^\gamma)^{1/\gamma}}$$

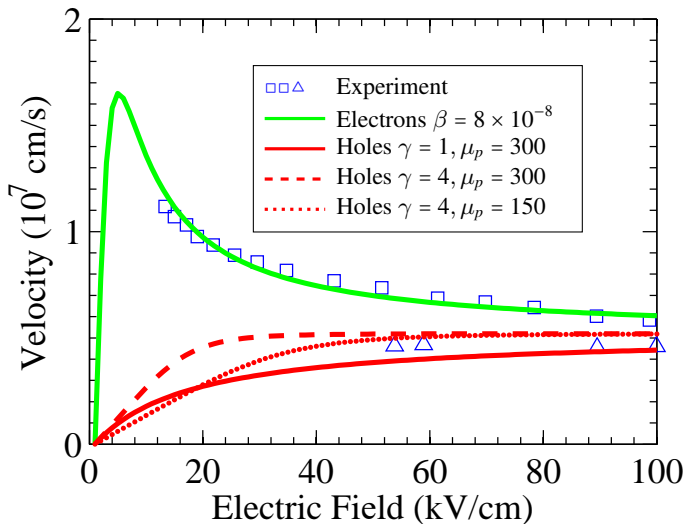
μ_n	: low-field electron mobility	μ_p	: low-field hole mobility
$v_{n,\text{sat}}$: saturated electron velocity	$v_{p,\text{sat}}$: saturated hole velocity
β	: fitting parameter	γ	: fitting parameter

¹M. Dentan and B. de Cremoux, *J. Lightw. Technol.* **8**, 1137–1144 (1990).

²K. W. Böer, *Survey of Semiconductor Physics* (Van Nostrand Reinhold, 1990).



Velocity of electrons and holes in InGaAs



¹T. H. Windhorn et al., J. Electron. Mater. **11**, 1065–1082 (1982).



Diffusion model

Empirical expressions that have been used to fit $D_n(\mathbf{E})$ for electrons¹ and $D_p(\mathbf{E})$ for the holes¹ are given by

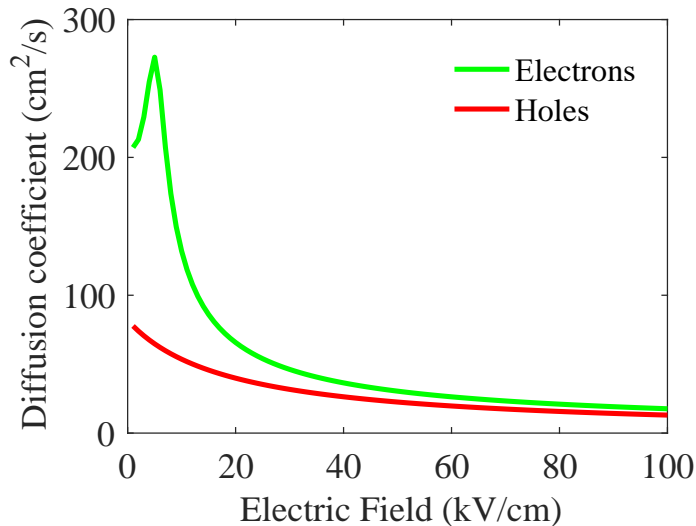
$$D_n(\mathbf{E}) = \frac{k_B T \mu_n / q}{\left[1 - 2 (|\mathbf{E}|/E_p)^2 + \frac{4}{3} (|\mathbf{E}|/E_p)^3\right]^{1/4}}, \quad D_p(\mathbf{E}) = \frac{k_B T}{q} \frac{\mathbf{v}_p(\mathbf{E})}{\mathbf{E}}$$

E_p : fitting parameter, 4×10^3 V/cm

¹K. J. Williams, "Microwave nonlinearities in photodiodes," PhD Dissertation, University of Maryland College Park, Maryland, USA, 1994.



Diffusion model



Recombination-Generation

- The largest contribution to recombination is the Shockley-Read-Hall (SRH) effect.
 - ▶ also known as trap-assisted nonradiative recombination
 - ▶ the expression for SRH recombination is

$$R = \frac{np - n_i^2}{\tau_p(n + n_i) + \tau_n(p + n_i)}$$

τ_n : electron lifetime

τ_p : hole lifetime

n_i : intrinsic doping concentration

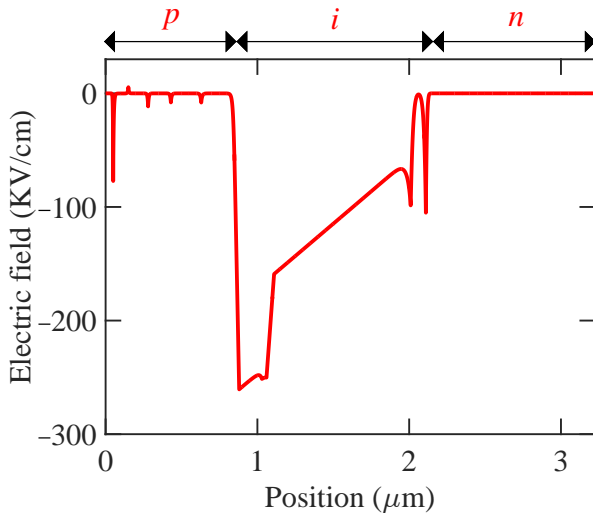
- The generation rate from impact ionization:

$$G_{ii} = \alpha_n \frac{|\mathbf{J}_n|}{q} + \alpha_p \frac{|\mathbf{J}_p|}{q}, \quad \alpha_{n,p} = A_{n,p} \cdot \exp \left[- \left(\frac{B_{n,p}}{|\mathbf{E}|} \right)^m \right]$$

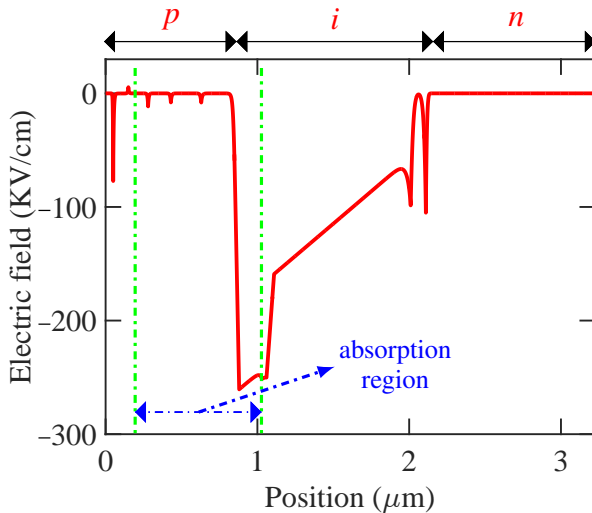
A_n, A_p, B_n, B_p, m : impact ionization parameters



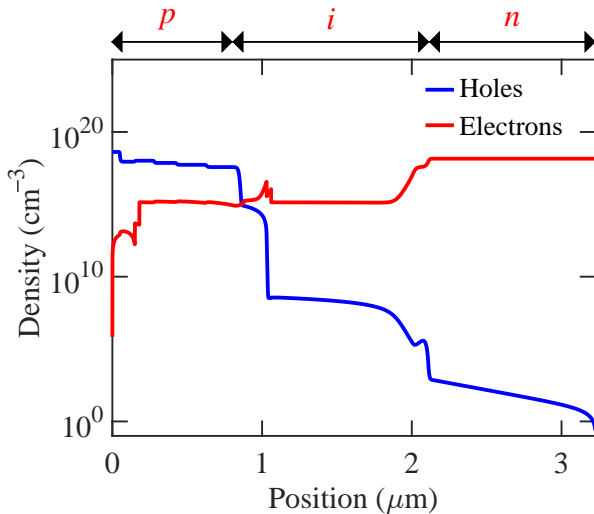
Electric field inside the MUTC photodetector



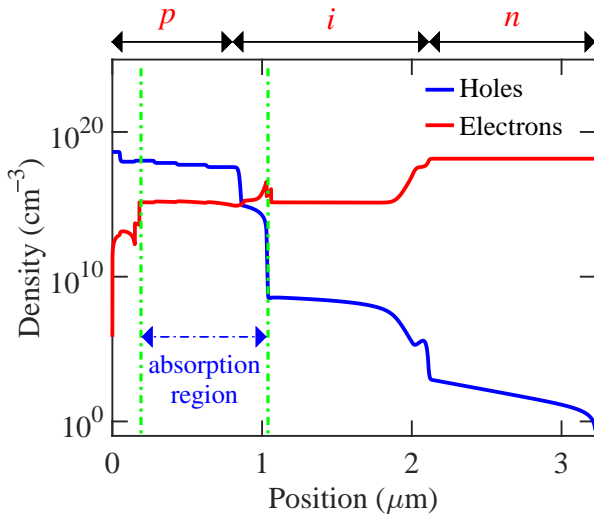
Electric field inside the MUTC photodetector



Carrier concentration inside the MUTC photodetector



Carrier concentration inside the MUTC photodetector



Calculation of the impulse response

- To calculate the impulse response,
 - ▶ we first calculate the steady state output current
 - ▶ we then perturb the optical generation rate and calculate the perturbed current
- The perturbed optical generation rate ΔG_{opt} is defined as

$$\Delta G_{\text{opt}} = rG_{\text{opt}} \operatorname{sech}\left(\frac{t}{\tau}\right)$$

- ▶ r = perturbation coefficient
- ▶ t = time
- ▶ τ = impulse width
- ▶ $\operatorname{sech}(x)$ = hyperbolic secant function



Calculation of the impulse response

- We define the normalized impulse response $h(t)$ as

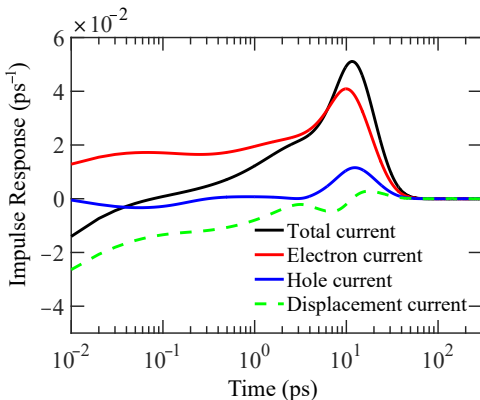
$$h(t) = \frac{\Delta I_{\text{out}}(t)}{\int_0^{\infty} \Delta I_{\text{out}}(t) dt}$$

- ▶ $\Delta I_{\text{out}}(t)$ = change in the output current due to the perturbed optical generation rate
- The transfer function $H(f)$ of the photodetector is defined as

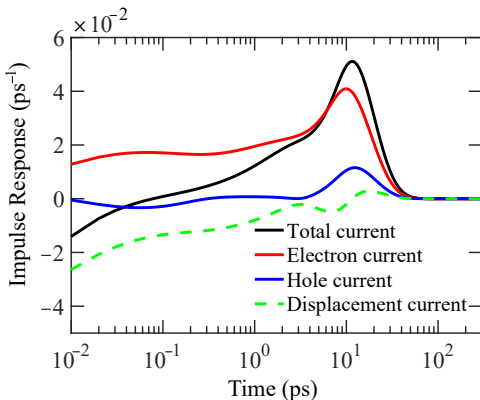
$$H(f) = \int_{-\infty}^{\infty} h(t) \exp(-2\pi jft) dt$$



Impulse response of the MUTC photodetector



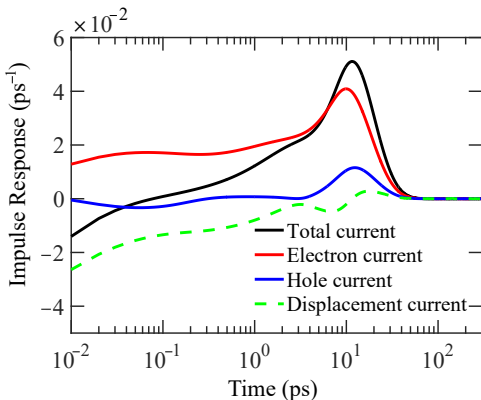
Impulse response of the MUTC photodetector



- The displacement current dominates the total current for the first 50 fs



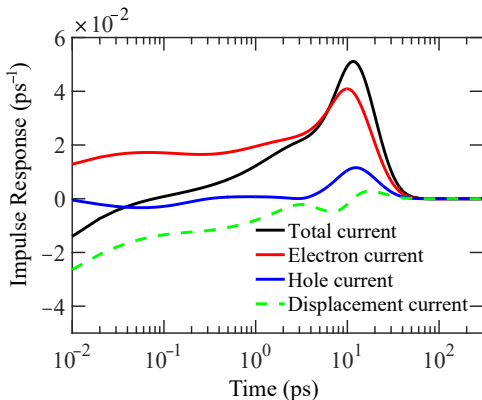
Impulse response of the MUTC photodetector



- The displacement current dominates the total current for the first 50 fs
- Thereafter, the electron current dominates at all times



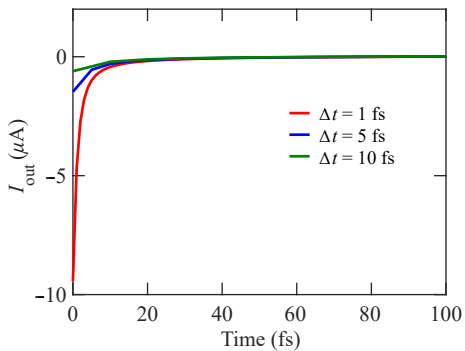
Impulse response of the MUTC photodetector



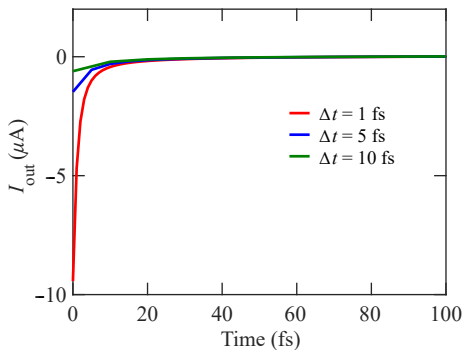
- The displacement current dominates the total current for the first 50 fs
- Thereafter, the electron current dominates at all times
- Hole current does not play a major role



Calculation of the impulse response



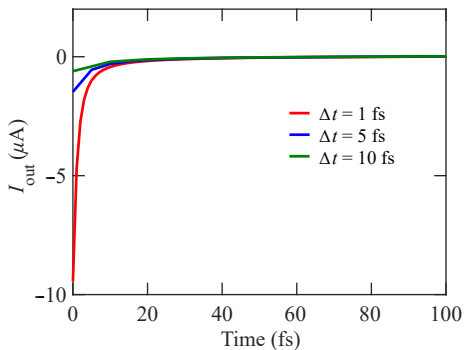
Calculation of the impulse response



- We compared three different time meshes Δt



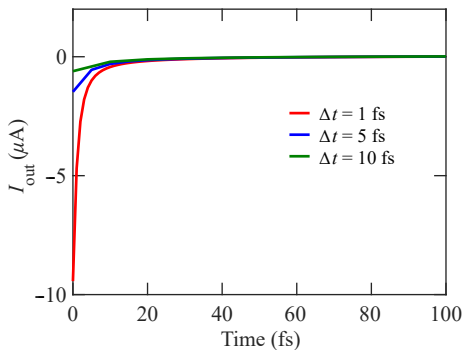
Calculation of the impulse response



- We compared three different time meshes Δt
- The results are almost identical for $t > 20$ fs



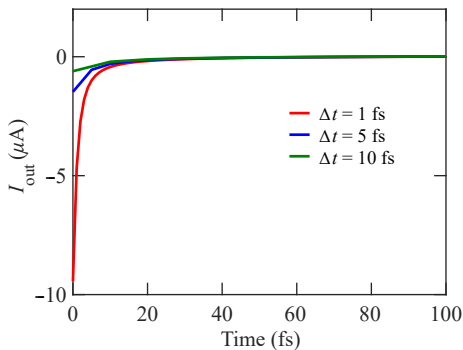
Calculation of the impulse response



- We compared three different time meshes Δt
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- The frequency dependence is reliable up to frequencies of 50 THz



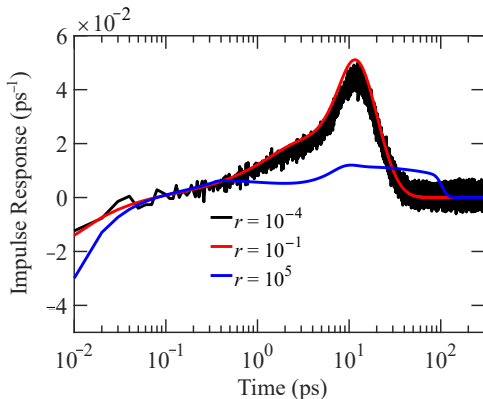
Calculation of the impulse response



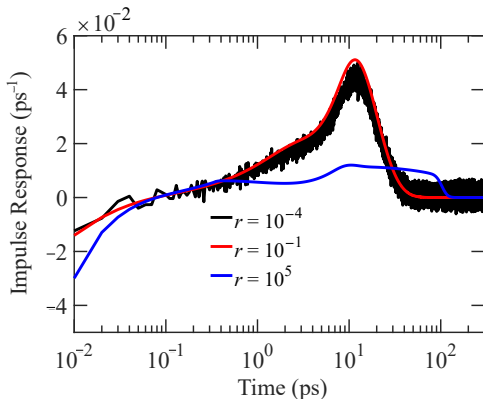
- We compared three different time meshes Δt
- The results are almost identical for $t > 20$ fs
- The frequency dependence is reliable up to frequencies of 50 THz
 - far beyond the device limit of 10–50 GHz



Calculation of the impulse response



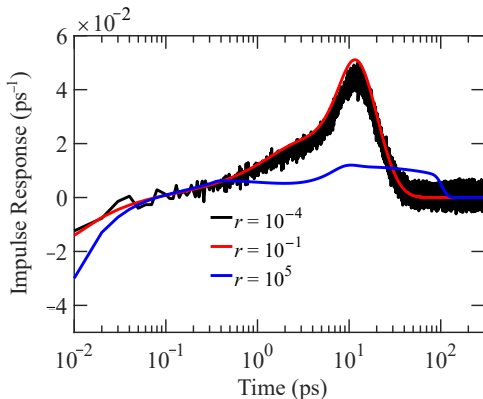
Calculation of the impulse response



- When $r = 10^{-4}$, computational errors degrade the impulse response



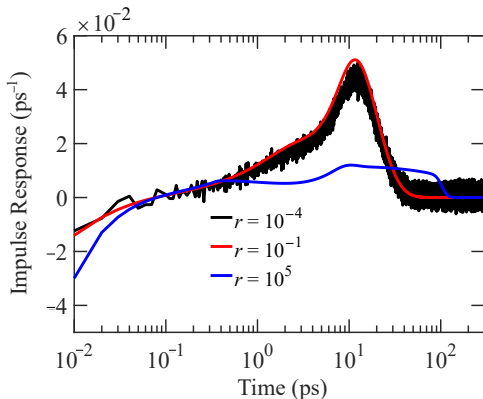
Calculation of the impulse response



- When $r = 10^{-4}$, computational errors degrade the impulse response
- When $r = 10^5$, nonlinearity distorts the impulse response



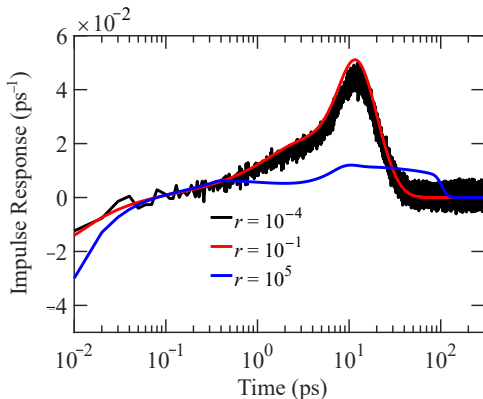
Calculation of the impulse response



- When $r = 10^{-4}$, computational errors degrade the impulse response
- When $r = 10^5$, nonlinearity distorts the impulse response
- For $10^{-3} < r < 10^4$, the impulse response is almost identical



Calculation of the impulse response



- When $r = 10^{-4}$, computational errors degrade the impulse response
- When $r = 10^5$, nonlinearity distorts the impulse response
- For $10^{-3} < r < 10^4$, the impulse response is almost identical
- We use $r = 10^{-1}$ in our calculations



Calculation of the phase noise

- The mean-square phase fluctuation is given by¹

$$\langle \Phi_n^2 \rangle = \frac{1}{N_{\text{tot}}} \frac{\int_0^{T_R} h(t) \sin^2 [2\pi n(t - t_c)/T_R] dt}{\left\{ \int_0^{T_R} h(t) \cos [2\pi n(t - t_c)/T_R] dt \right\}^2}$$

- ▶ N_{tot} = total number of electrons in the photocurrent
- ▶ t_c = central time of the output current
- ▶ T_R = repetition time between optical pulses
- In the limit of short optical pulse widths (≤ 500 fs):
 - ▶ $\langle \Phi_n^2 \rangle$ tends to a non-zero constant

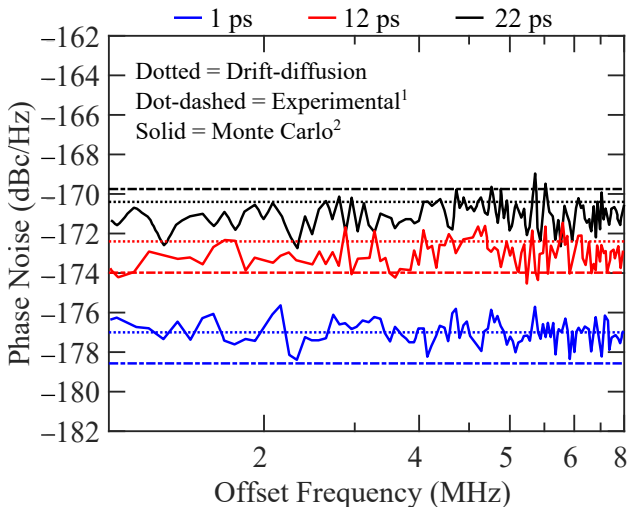
$$\langle \Phi_n^2 \rangle = \frac{1}{N_{\text{tot}}} \frac{\int_0^{T_R} h_e(t) \sin^2 [2\pi n(t - t_c)/T_R] dt}{\left\{ \int_0^{T_R} h_e(t) \cos [2\pi n(t - t_c)/T_R] dt \right\}^2}$$

★ $h_e(t)$ = electronic impulse response of the device

¹S. E. Jamali Mahabadi et al., Opt. Express **27**, 3717–3730 (2019).



Phase noise in the MUTC photodetector

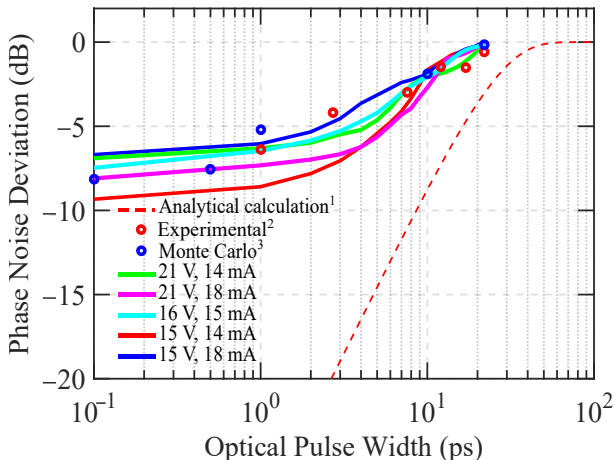


¹F. Quinlan et al., Nat. Photonics **7**, 290–293 (2013).

²W. Sun et al., Phys. Rev. Lett. **113**, 203901 (2014).



Phase noise in the MUTC photodetector



¹F. Quinlan et al., J. Opt. Soc. Am. B **30**, 1775–1785 (2013).

²F. Quinlan et al., Nat. Photonics **7**, 290–293 (2013).

³W. Sun et al., Phys. Rev. Lett. **113**, 203901 (2014).



Conclusions

- We used the drift-diffusion equations to calculate
 - the impulse response
 - the phase noisein an MUTC photodetector with short optical pulses
- We found excellent agreement with prior experiments¹ and Monte Carlo simulations²
- Advantages of our approach
 - orders of magnitude faster than Monte Carlo simulations
 - enables device optimization
 - physical insight
- We determined the parameters for simulating photodetectors in pulse mode
 - drift and diffusion velocity coefficients
 - mesh size and time step

¹F. Quinlan et al., Nat. Photonics **7**, 290–293 (2013).

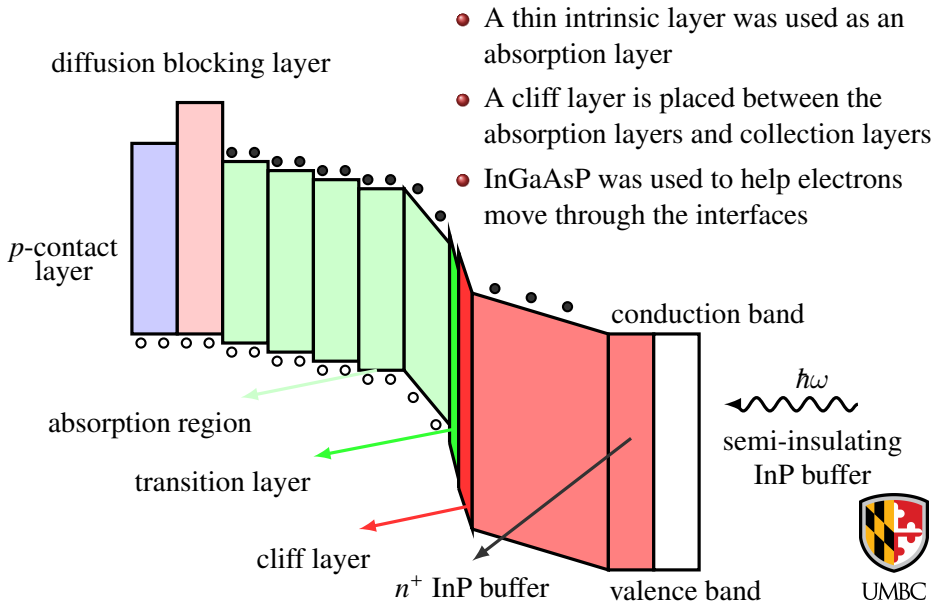
²W. Sun et al., Phys. Rev. Lett. **113**, 203901 (2014).



Thank you for your attention

Backup slides

Structure of an MUTC photodetector



Implicit method

Fully implicit method¹ (backwards Euler method) is used to solve the equations

$$\frac{n^{t+1} - n^t}{\Delta t} = F_n(n^{t+1}, p^{t+1}, \varphi^{t+1})$$

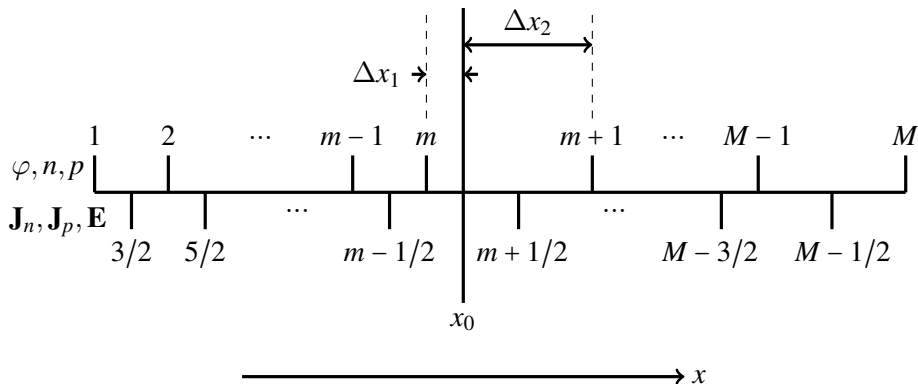
$$\frac{p^{t+1} - p^t}{\Delta t} = F_p(n^{t+1}, p^{t+1}, \varphi^{t+1})$$

$$0 = F_\varphi(n^{t+1}, p^{t+1}, \varphi^{t+1})$$

¹S. Selberherr, *Analysis and simulation of semiconductor devices*.
New York: Springer-Verlag Wien, 1984.



Modeling Approach (1D Scheme)



Gridding scheme used in device model for multilayer devices

- φ, n, p are defined at integer grid values
- $\mathbf{J}_n, \mathbf{J}_p, \mathbf{E}$ are defined at half-integer grid values



Phase Noise

- We define the finite-time Fourier transform,

$$F_T\{x(t)\} \equiv \int_{-T/2}^{T/2} x(t) \exp(-j2\pi ft) dt$$

- We next write

$$\begin{aligned} F_T\{i(t)\} &= \int_{-T/2}^{T/2} i(t) \exp(-j2\pi ft) dt \\ &= \frac{1}{2K} \sum_{k=-K}^{K-1} \int_0^{T_R} i(t + kT_R) \exp[-j2\pi f(t + kT_R)] dt \end{aligned}$$

- ▶ $i(t)$ = output current
- ▶ T_R = repetition time between optical pulses
- ▶ $T = KT_R$



Phase Noise

- If we let $i_k(t) = i(t + kT_R)$, so that $i_k(t)$ is the k -th current output pulse, we obtain

$$F_T\{i(t)\} = \frac{1}{2K} \sum_{k=-K}^{K-1} \int_0^{T_R} i_k(t) \exp(-j2\pi ft) dt$$

- For the n -th harmonic of the current, we obtain

$$R_n + jQ_n = \frac{1}{2K} \sum_{k=-K}^{K-1} \int_0^{T_R} i_k(t) [\cos(2\pi n f_r t) - j \sin(2\pi n f_r t)] dt$$

- ▶ R_n = in-phase component of the n -th harmonic
- ▶ Q_n = quadrature component of the n -th harmonic



Phase Noise

- We also define the ensemble average $\langle c_k(t) \rangle$ for any quantity $c_k(t)$ as

$$\langle c_k(t) \rangle \equiv \lim_{K \rightarrow \infty} \frac{1}{2K} \sum_{k=-K}^{K-1} c_k(t)$$

It is useful to shift the time to remove the quadrature component to good approximation

$$R_n + jQ_n = \frac{1}{2K} \sum_{k=-K}^{K-1} \int_0^{T_R} i_k(t) \left\{ \cos \left[\frac{2\pi n}{T_R} (t - t_c) \right] - j \sin \left[\frac{2\pi n}{T_R} (t - t_c) \right] \right\} dt$$

- t_c = central time of the output current



Phase Noise

- t_c is defined by

$$Q_n = \int_0^{T_R} \langle i_k(t) \rangle \sin \left[\frac{2\pi n}{T_R} (t - t_c) \right] dt = 0$$

- We define

$$\Phi_n = \frac{-j \sum_{k=-K}^{K-1} \int_0^{T_R} i_k(t) \sin \left[\frac{2\pi n}{T_R} (t - t_c) \right] dt}{\sum_{k=-K}^{K-1} \int_0^{T_R} i_k(t) \cos \left[\frac{2\pi n}{T_R} (t - t_c) \right] dt} = 0$$



Phase Noise

- Although we have $\Phi_n = 0$, the separate phase contributions of each comb pulse to Φ_n will be non-zero. We have $\Phi_n = \sum_k \Phi_{kn}$ and $Q_n = \sum_k Q_{kn}$, where

$$\Phi_{kn} = \frac{Q_{kn}}{R_n} = \frac{-j \int_0^{T_R} i_k(t) \sin \left[\frac{2\pi n}{T_R} (t - t_c) \right] dt}{\int_0^{T_R} i_k(t) \cos \left[\frac{2\pi n}{T_R} (t - t_c) \right] dt}$$

- We find

$$\Phi_{kn}^2 = \frac{\int_0^{T_R} \int_0^{T_R} i_k(t) i_k(u) \sin \left[\frac{2\pi n}{T_R} (t - t_c) \right] \sin \left[\frac{2\pi n}{T_R} (u - t_c) \right] dt du}{\left\{ \int_0^{T_R} i_k(t) \cos \left[\frac{2\pi n}{T_R} (t - t_c) \right] dt \right\}^2}$$



Phase Noise

- We may assume that the electrons in each current pulse are Poisson-distributed
- This assumption may seem surprising at first since the photodetectors of interest to us operate in a nonlinear regime
- The electrons only interact through the electric field that they collectively create
- Due to the large number of electrons that create this field, a mean-field approximation is valid, and the arrival time of the electrons is nearly independent
- Given the assumption that the current pulses are Poisson-distributed, we find

$$\langle i_k(t)i_k(u) \rangle - \langle i_k(t) \rangle \langle i_k(u) \rangle = h(t)e^2 N_{\text{tot}} \delta(t - u)$$

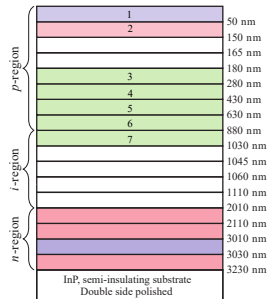
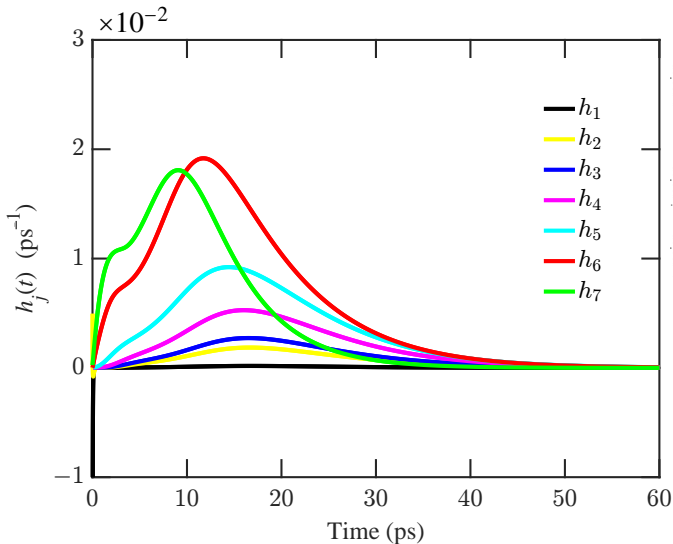


Device optimization

- Our goal is to reduce the tails in the impulse response
 - A long tail in the impulse response translates to higher phase noise
- We first altered the thickness of each absorption layer up to 10%
 - no significant change 😞
- We next altered the doping density in each of the absorption layers
 - a smaller tail and lower phase noise 😊



Device optimization



$$h(t) = \sum_{j=1}^N h_j(t),$$



Device optimization

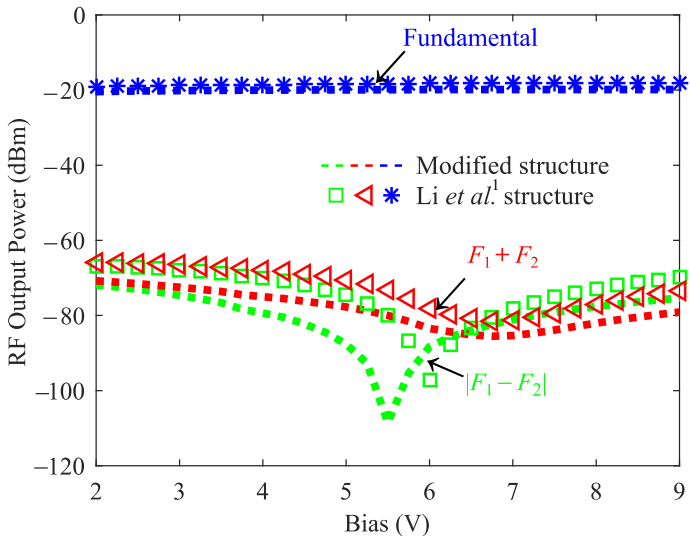
- Phase Noise 1 = phase noise of the Li et al.¹ structure
- Phase Noise 2 = phase noise of the modified structure
- Difference = (Phase Noise 1) – (Phase Noise 2)

Pulse Width	Original structure	Modified structure	Difference
1 ps	-178.6 dBc/Hz	-180.0 dBc/Hz	1.4 dBc/Hz
12 ps	-174.0 dBc/Hz	-175.5 dBc/Hz	1.5 dBc/Hz
22 ps	-169.7 dBc/Hz	-172.8 dBc/Hz	3.1 dBc/Hz

¹Z. Li et al., IEEE J. Quantum Electron. **46**, 626–632 (2010).



Device optimization



¹Z. Li et al., IEEE J. Quantum Electron. **46**, 626–632 (2010).

